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THERMAL/PHYSICAL PROPERTIES

- 1. BOILING POINT-Should be lower than operating conditions
- 2. DISCHARGE TEMPERATURE-Should be lower than 130°C
- 3. DISCHARGE PRESSURE-Should be reasonably low
- 4. SPECIFIC VOLUME-Should be low
- 5. DENSITY-Should be high
- 6. Latent heat of vaporization-Should be high
- 7. Compressor displacement-Should be low

- REFRIGERANT EVALUATION PROCESS
- 1. ENVIRONMENTAL IMPACT
- 2. PERFORMANCE-COP-(Output in kW /input in kW)
- 3. ENERGY EFFICIENCY-Energy consumed -kW/TR
- 4. TOXICITY/SAFETY
- 5. FLAMMABILITY
- 6. MATERIAL COMPATIBILITY
- 7. STABILITY
- 8. COST



ABOVE ALL OTH	L REFRIGERANT SCORES HER REFRIGERANTS
Ammonia is produced in a n animals; 17 grams/d	atural way by human beings and lay produced by humans.
Natural production	3000 million tons/year
Natural production Production in factories	3000 million tons/year 120 million tons/year

Ammonia Refrigerat	tion-Grade properties
Boiling point at one atmosphere(101.33kPa)	-33.33 Deg. C
Freezing point/Triple point at one atmosphere	-77.66 Deg. C
Critical Temperature	132.22 Deg. C
Relative Density of Vapour compared to air	0.5976-Lighter than air
Lower Flammability limit-LFL	15-16%-108000mg/m3
Upper Flammability limit	25-28%-240,000mg/m3
Ignition temperature	651.1 Deg. C
Ratio of sp. heat at 15 ⁰ C and 1 atmosphere (Y=C _p /C _v)	1.32
Solubility in water	0.571kg or 650 g in 1 ltr. of water



mmonia content	Min.99.95%-purity
ppearance	Colourless
dour	Characteristic-Pungent
P	0
WP	0
mospheric life	Nearly zero <0.019165
ter content	33PPM max.
l content	2PPM max.
n condensable	0.2ml/g
lt content	Nil
ridine, Hydrogen sulphide, Naphthalene	Nil
lecular weight	17.031
oncentration in Human blood	0.8-1.7 PPM







Refrigerant	ODP	GWP	Atmospheric Life-years
R-22 (HCFC -22)	0.055	1790	11.9
R-134a	0	1370	13.4
R404A	0	3700	16
R407C	0	1700	5.6
R410A	0	2100	16
R507C	1	3300	40.5
R32	0	675	4.9
R290-Propane	0	3.3	12.0
R1234Ze	0	6.0	0
R1234yf	0	4.0	0
R744=CO2	0	1.0	29-36
Ammonia, R717	0	0	<0.02

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TEWI Effect--Total Equivalent Warming Impact

It is defined as sum of the direct emissions from leaks and indirect emissions (energy use) resulting from power consumption.

TEWI can be calculated using the equation below (UNIDO 2009): TEWI = direct emissions + indirect emissions =

- $(GWP \times L \times N) + (Ea \times \beta \times n)$, where
- L- annual leakage rate in the system, kg (3% of refrigerant charge annually),
- N life of the system, years (15 years),

n - system running time, years (based on weather data, 4910 hours), Ea - energy consumption, kWh per year (modelled for each

- refrigerant),
- β carbon dioxide emission factor, CO2-eq. emissions per kWh (165 g CO2/kWh)



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What is TEWI?

TEWI is a measure of the global warming impact of equipment based on the total related emissions of greenhouse gases during the operation of the equipment and the disposal of the operating fluids at the end-of-life.

TEWI takes into account both direct emissions, and indirect emissions produced through the energy consumed in operating the equipment. TEWI is measured in units of mass in kg of carbon dioxide equivalent (CO2-e).

TEWI is calculated as the sum of two parts, they are:

1. Refrigerant released during the lifetime of the equipment,

including unrecovered losses on final disposal,

2. The impact of CO2 emissions from fossil fuels used to generate energy to operate the equipment throughout its lifetime., means related to power consumption





EWI- COM for an <u>c</u> tempera	PARISON evaporation ture $t_c=35$ °C	OF DIFFER temperature <i>t</i> C, and an ope	ENT REFR $t_0 = -20^\circ$, a contracting time of	RIGERANT ondensing of 15 years.
	Direc	t Effect	Indire	et Effect
Table 3	s● Operating Leak (kg CO2)	Fluid Recovery Leak (kg CO2)	Drive Energy Generation (kg CO2)	TEWI (kgCO2)
R22	1,033,500	68,900	1,805,400	2,907,800
R134a	911,625	60,775	1,884,150	2,856,550
R407C	999,352	66,623	2,104,650	3,170,625
R410A	1,049,555	69,970	1,962,900	3,082,425
R717	0	0	1,457,550	1,457,550
			. ,	

What is LCCP?

LCCP = Life Cycle Climate Performance

TEWI +1+2

1. GWP (indirect; energy consumption from chemical Refrigerant production and transport, manufacturing components,

assembly and end-of-life) 2 GWP (direct; chemical refrigerant emissions including

atmospheric reaction products, manufacturing leakage and end-oflife)

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IT IS THE LATENT HEAT WHICH MAKES **REFRIGERATION SYSTEMS WORK-(PHASE CHANGE)**

-SENSIBLE HEAT DOES HARDLY ANY COOLING

When refrigerant boils in the Evaporator it absorbs lot of heat from the medium to be cooled and gets converted in vapour , i.e. latent heat.

For Example- at -10°C, the enthalpy of Ammonia liquid is 1450.70kJ/kg whereas specific heat of liquid is only 4.564 kJ/kg.K, Latent heat is nearly 320 times more

Same thing happens in condenser when vapours get condensed in liquid it rejects lot of heat.



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LATENT HEAT COMPARISON @ 4-5°C

•	Water R-	718-	2489	.04kJ/kg
---	----------	------	------	----------

- Ammonia R717-1247.85kJ/kg
- R410A-
- 214.48kJ/kg • HCFC 22/R22-201.79kJ/kg
- HFC 134a/R134a-
- 195.52kJ/kg • R404A-162.03kJ/kg

Ammonia latent heat is 6 to 9 times more





n .							,15	1 4010	0-2			
Refi	rigerants											29.9
	Tal	ble 9 Con	nparative	Refrige	rant Per	forman	ce per T	on of Refr	igeration			
No.	Refrigerant Chemical Name or Composition (% by mass)	Evap- orator Pressure, psia	Con- denser Pressure, psia	Com- pression Ratio	Net Refrig- erating Effect, Btu/lb	Refrig- erant Circu- lated, Ib/min	Liquid Circu- lated, gal/min	Specific Volume of Suction Gas, ft ³ /lb	Com- pressor Displace- ment, gal/min	Power Consump- tion, hp	Coeffi- cient of Perform- ance	Com- pressor Discharge Temp., °F
170	Ethane	233.2	672.8	2.88	69.5	0.81	0.35	0.541	3.27	0.489	2.7	121.73
744	Carbon dioxide	326.9	1041.4	3.19	57.3	0.51	0.10	0.269	1.03	0.257	2.69	157.73
1270	Propylene	51.9	189.1	3.64	123.0	0.46	0.11	2.081	7.12	0.295	4.5	107.33
290	Propane	41.5	155.9	3.76	119.5	0.47	0.12	2.502	8.73	0.292	4.5	96.53
502	R-22/115 (48.8/51.2)	49.7	190.3	3.83	45.6	1.25	0.13	0.814	7.59	0.306	4.38	100.13
507A	R-125/143a (50/50)	55.0	211.6	3.85	47.4	1.20	0.14	0.814	7.31	0.321	4.18	94.73
404A	R-125/143a/134a (44/52/4)	52.9	206.0	3.89	49.1	1.16	0.14	0.860	7.45	0.318	4.21	96.53
410A	R-32/125 (50/50)	69.3	271.5	3.92	72.2	0.77	0.09	0.873	5.04	0.298	4.41	123.53
125	Pentafluoroethane	58.5	226.4	3.87	36.7	1.51	0.16	0.631	7.12	0.327	3.99	87.53
22	Chlorodifluoromethane	42.8	172.2	4.02	69.9	0.81	0.08	1.248	7.58	0.287	4.66	127.13
12	Dichlorodifluoromethane	26.3	107.5	4.09	50.3	1.12	0.10	1.479	12.43	0.284	4.7	100.13
500	R-12/1528 (73.8/26.2)	31.0	127.1	4.09	60.1	0.94	0.10	1.504	10.54	0.284	4.00	105.53
40/0	R-32/125/134a (23/25/52)	41.8	182.7	4.38	70.2	0.81	0.09	1.289	7.80	0.298	4.5	118.13
124-	Isobutane*	12.8	38.5	4.58	113.5	0.50	0.11	0.524	24.30	0.288	4.02	85.73
1348	Tedratiuoroetnane	23.0	111.2	4.71	63.6	0.89	0.09	1.945	12.90	0.290	4.0	98.33
124	Chiorotetrafiuoroetnane*	12.8	64.3	5.05	50.7	1.11	0.10	2.741	22.81	0.287	4.02	85.73
(00	Determine	34.1	41.0	4.94	4/4.3	0.12	0.02	0.197	26.04	0.282	4.70	209.93
	Tricklass Occurrently and	3.0		6.05	67.0	0.47	0.07	10.323	77.60	0.292	4.74	100.13
122	Disklasstai0ssasthana	2.9	16.0	6.01	61.2	0.02	0.02	14 270	00.21	0.274	4.0	01.12
123	Trish lanotsi (han stathan st	1.0	13.8	0.81	01.2	0.93	0.08	14.279	99.21	0.274	4.7	91.13

COMPARISON@-+40°C/-5°C (for cold storage application)					
Refrigerant	Capacity-kW	Power consumption-kW	С.О.Р.		
Ammonia-R717	1068.731	215.255	4.965		
R410A	159.327	32.416	4.80		
R134a	138.124	29.551	4.67		
R404A	102.346	25.142	4.07		
R22	153.832	32.416	4.74		
Propane-R290	263.01	56.917	4.62		
R507	109.137	25.096	4.35		
Isobutate-R600a	253.671	52.966	4.79		
Water -R718	2324.327	525.501	4.42		
CO ₂ -(+31/-5)	107.718	35.701	3.02		

COMPARISON@-+40°C/+2°C (for chilled water application)

Refrigerant	Capacity-kW	Power consumption-kW	C.O.P.
Ammonia-R717	1076.335	173.473	6.20 -
R410A	155.467	28.647	5.43
R134a	142.197	24.201	5.88
R404A	106.254	20.530	5.18
R22	156.419	26.376	5.93
Propane-R290	290.557	46.659	5.80
R507	111.904	20.452	5.47
Isobutate-R600a	263.125	43.728	6.02
Water -R718	2337.240	403.211	5.80
CO ₂ -(+31 ⁰ C/-5 ⁰ C)	104.106	26.692	3.90

COMPARISON@-+40°C/-25°C (for frozen storage application)					
Refrigerant	Capacity-kW	Power consumption-kW	C.O.P.		
Ammonia-R717	1043.211	358.501	2.91		
R410A	142.662	57.08	2.50		
R134a	126.048	46.768	2.70		
R404A	90.272	39.978	2.26		
R22	145.666	52.230	2.79		
Propane-R290	240.649	89.845	2.68		
R507	100.675	40.348	2.50		
Isobutate-R600a	226.378	82.130	2.76		
Water -R718	2287.299	1024.183	2.23		
CO ₂ -(+31/-5)	111.222	66.772	1.67		

(for blast/plate/ spiral freezing)						
Refrigerant	Capacity-kW	Power consumption-kW	C.O.P.			
Ammonia-R717	1020.824	496.672	2.06			
R410A	80.654	53.063	1.52			
R134a	116.693	61.965	1.88			
R404A	80.854	53.063	1.52			
R22	138.945	70.159	1.98			
Propane-R290	223.32	118.890	1.88			
R507	93.932	54.234	1.73			
Isobutate-R600a	207.398	107.450	1.93			
Water –R718	2259.468	1603.402	1.41			
CO2-(+31/-40)	109.446	96.160	1.14			

Energy	efficiency -	Reciproca	ating	compr
Performance	: t-evap,. = -10	°C; t-cond. = 3	35 °C	
Refrigerant	Refrigerating	Shaft power	СОР	1/COP
	capacity			
[-]	[kW]	[kW]	[-]	[%]
R717 (NH ₃)	425.8	112.9	3.771	100.0
R22	380.3	121.3	3.135	120.3
R134a	218.8	74.7	2.929	128.7
R404A	352.4	132.6	2.658	141.9
R507	356.7	136.0	2.62	143.8



1	refrigerants	for various	application	S
Refrigerant	For positive Temperature cold rooms- +40°C/+2°C	For secondary fluids operation +40°C/-5°C	For low temperature cold rooms- +40 ⁰ C/-25 ⁰ C	Blast freezers/IQF +40ºC/-40ºC
Ammonia -R717	6.20	4.965	2.91	2.06
R410A	5.43	4.80	2.50	1.75
R134a	5.88	4.67	2.70	1.88
R404A	5.18	4.07	2.26	1.52
R22	5.93	4.74	2.79	1.98

ressor	v comp	cy – Screv	rgy efficien	Ene
С	nd. = 35 ° (-30 ° C; t-cor	Temperature.	t-evaporating
1/COP	COP	Shaft	Refrigerating	Refrigerant
		power	capacity	
[%]	[-]	[kW]	[kW]	[-]
100.0	1.912	228.0	435.9	R717 (NH₃)
98.6	1.940	228.4	443.2	R22
120.3	1.589	139.4	221.5	R134a
124.7	1.533	257.5	394.7	R404A
123.0	1.555	262.7	408.4	R507

DENSITY		
REFRIGERANT	molecular weight	
Ammonia-R717	17.02-lighter than air	
AIR-R729	28.96	
R290-Propane	44.097	
R410A	72.60	
R404A	72.60	
R-22	86.468	
R134a	102.03	
1234yf/1234ze	114.0	

From the above table one can see that Ammonia is the only refrigerant lighter than air, and all other refrigerants are heavier than air

AMMONIA IS LIGHTER THAN AIR & HAS LOWER DENSITY

All other refrigerants are heavier than air and have higher density If ammonia leaks- it rises in the air and disintegrated-other refrigerants settle in the machine room and displace oxygen.

If machine room is not ventilated there have been more accidents reported due to loss of oxygen leading to suffocation

People are unable to detect leakages of these refrigerants as they have no smell and leakage is suspected only when cooling effect is reduced or lost.

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HEAT TRANSFER RATE AND CONDUTIVITY

The disadvantage of heavier refrigerants is the heat transfer rate is lower during evaporation and condensation partly as a result of a greater liquid film thickness due to lower evaporation or condensation enthalpy.

Further disadvantage, is the very low thermal conductivity of HCFC and HFC refrigerants in the liquid phase as compared with ammonia in the liquid phase.

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Most of the thermal properties influencing heat transfer are favorable to ammonia compared to HCF 22 refrigerant. The heat transfer properties of R134a and R404A are very similar to R-22 Specific heat of liquid is nearly 4 times -4 to 1 Latent heat of vaporization is-6 to 1 Liquid thermal conductivity is -5.5 to 1 Viscosity is less-0.8 to1 Liquid density is less as mentioned earlier-0.5 to 1 All these properties help in improving heat transfer correlation between ammonia relative to HCFC 22 and other commonly used manmade refrigerants for condensing and evaporating heat transfer processes.

Leakage losses

- 1. The molecular weight of ammonia is 17.03, whereas HCFC 22 has 86.48, R134a is 102.03, R404A is 97.604 & R410A is 72.585.
- 2. This means if plant develops leak of equal size on both plants, loss of higher density refrigerants would be greater than ammonia.
- 3. Similarly, during purging the loss of refrigerant is less in ammonia plants compared to other refrigerants for the same reason.

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Heat transfer rates or R134a	of Ammonia compar or R404A refrigeran	ed to R-22 t.
	Ammonia	R-22, R134a,
		R404A
Condensation outside	7500-11000	1700-2800
tubes (W/m ² K)		
Condensation inside tubes	4200-8500	1400-2000
(W/m ² K)		
Boiling outside Tubes	2300-4500	1400-2000
(W/m ² K)		
Boiling inside tubes	3100-5000	1500-2800
(recirculation of liquid)		
(W/m^2K)		
higher heat transfer coefficients fo	r Ammonia, helps in use of s	maller evaporators &
condensers or retain same heat tra	nsfer areas & operate at high	her evaporating
efficiency/C.O.P.	temperatures, thus improvin	g the cycle



HCFC 22 & other HFC refrigerant liquids and commonly used lubricating oils are mutually soluble in varying degrees depending upon type of oil, operating temperature and pressure,

Ammonia & oil are virtually insoluble. Hence recovering oil from various parts of ammonia system is easier & requires different approach to oil management. Oil recovery problems are nonexistent with ammonia at partial loads unlike HCFC 22 systems.

Also piping design is simpler in ammonia since oil is immiscible and hence does not require double risers or complicated piping arrangement to ensure that oil is returning to the compressor by maintaining adequate velocities even at partial loads and ensuring no oil traps anywhere in piping design.

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Volum co	e and ma ndensing	and -15	rate for ⁰ C evap	100kW ca orating te	apacity mperat	at 40ºC ure
Refrigerant	Cap.kW	Power kW	С.О.Р.	Pressure ratio	Mass flow- kg/hr.	Volume flow- m ³ /hr.
Ammonia R- 717	100	26.686	3.75	6.583	<u>340.704</u>	173.0421
R-22	100	27.897	3.58	6.5186	2401.91	186.4804
R134a	100	28.583	3.50	6.193	2723.76	326.6467
R404A	100	33.418	2.99	4.955	3732.48	204.5811

Ammonia refrigerant's mass flow rate is 1/7 times that of HCFC 22, or 10.97 times less compared to R404A -only 1/7 liquid needs to be pumped if R22 is used or 10 times lower pump-power compared to R404A. Thus, mechanical pumping power will be much less in ammonia system.

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Refrigeration capcity for +40 ⁰ C condensing and + 5 ⁰ C
evaporating Temperature say for 50mm pipe size-
Ref: ASHRAE 2014 Refrigeration volume

50mm R22 106.4 150.5 707.5 R134a 70.10 106 546 R404A 96.18 137.33 758.2 R410A 160.19 229.98 1320.9 <u>R717-</u> <u>218.6</u> <u>374.7</u> <u>2840.5</u>	Line size	Refrigerant	Suction line-kW	Discharge line - kW	Liquid line-kW
R134a 70.10 106 546 R404A 96.18 137.33 758.2 R410A 160.19 229.98 1320.9 <u>R717-</u> 218.6 374.7 2840.5 <u>Ammonia</u> 240.5 2840.5 2840.5	50mm	R22	106.4	150.5	707.5
R404A 96.18 137.33 758.2 R410A 160.19 229.98 1320.9 <u>R717-</u> 218.6 374.7 2840.5 <u>Ammonia</u> 210.9 200.9 200.9		R134a	70.10	106	546
R410A 160.19 229.98 1320.9 R717- Ammonia 218.6 374.7 2840.5		R404A	96.18	137.33	758.2
<u>R717-</u> <u>218.6</u> <u>374.7</u> <u>2840.5</u>		R410A	160.19	229.98	1320.9
		<u>R717-</u> Ammonia	<u>218.6</u>	374.7	<u>2840.5</u>

1	teat pump ap	oplications –te and higher he	o get highest h eat recovery	ot water
Refrigerant	Critical Temp⁰C	Critical pressure- MPa	Boiling point- ⁰ C	Critica Density kg/m3
R717-	132.25	11.333	-33.33	225.0
R134a	100.06	4.0593	-26.07	511.0
R22	96.15	4.99	-40.81	523.8
R1234yf	94.7	3.3822	-29.49	475.6
R32	78.11	5.782	-51.65	424.0
R404A	72.05	3.729	-46.22	486.5
R410A	71.36	4.903	-51.55	459.5
R744	30.98	7.377	-	467.6

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Pipe Si Cap	ze Comparison- acity -200kW, evap	ASHRAE –Refrige oorating temperatu	eration 2014 are +5ºC
Refrigerant	Suction line – mm OD	Discharge Line- mm OD	Liquid line – mm OD
Ammonia – R717	<u>50</u>	<u>40</u>	<u>20</u>
HCFC-22	80	65	32
HFC134a	80	80	40
R404A	80	65	40
R410A	65	50	32
PIPING,FITT	INGS COST AND OTHER R	INSULATION COS EFRGERANTS	ST IS MORE FOR

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Tolerance to water contamination

- 1. Ammonia systems are more tolerant to water contamination than HCFC/HFC systems.
- 2. A little leak of moisture in the system which does not exceed concentration beyond 100 PPM stays in the solution & does not freeze out.
- 3. Hence modest contamination with water does not usually interfere with ammonia system operation.
- 4. It is suggested that a small amount of water added in the ammonia system will help to reduce the risk of stress corrosion cracking.

Refrigerant	Cost per Kg as on 08-04-2020	Cost of oil per liter
Ammonia-R717	<u>Rs. 60</u>	<u>Rs.160</u>
R134a	Rs. 450	Rs.1350
R404A	Rs. 450	Rs. 1350
R410A	Rs. 450	Rs.1350

AMMONIA CONVINCES WITH TOP ENERGY **EFFICIENCY**

- 1. Zero ODP
- 2. Near Zero GWP-Zero Atmospheric Life
- Best Thermodynamic Efficiency compared to any other Refrigerant
 Favourable TEWI balance with high COP
- 5. Low cost
- 6. Lubricating oil inexpensive
- 7. Equipment manufactured in India- Compressors, condensers,
- evaporators
- 8. Available in all parts of country
- 9. Refrigerant Manufactured in India
- 10. Lighter than Air -Escapes to atmosphere and does not accumulate in machine room
- 11.Leaks easily detectable
- 12. Does not mix with oil-can be drained easily

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LIMITATIONS & DRAWBACKS

- 1. Toxicity
- 2. Flammability
- 3. Material compatibility
- 4. High Discharge temperature
- 5. OIL Miscibility

AMMONIA SMELLS-EASY LEAK DETECTION

Ammonia has a pungent odor and even small leaks as low as 5 PPM are detectable by smell so that maintenance staff can correct them. Almost all human beings can detect levels up to 25 PPM easily The smell is in fact an advantage since the smallest leakages are discovered immediately and then corrected.

The odourless refrigerants like HCFC-22 or HFC-134a and others, even if they leak from the system in large quantity, it won't be noticed till cooling performance drops. In case of leaks, since HFC/HCFC refrigerants are heavier than air & due to their odourless character, they settle down in plant room & more accidents have been reported due to suffocation.

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Flammability in Air @ 60°C & 101.3 kPa ASHRAE Standard Safety Group Higher Flammability A3 B3 LFL or ETFL60 $\leq 100 \text{ g/m}^3 \text{ OR HOC} \geq 19 \text{ MJ/kg}$ Lower Flammability A2 B2 LFL or ETFL60 > 100 g/m³ & HOC < 19 MJ/kg Lower Flammability LFL or ETFL60 > 100 g/m³ & HOC < 19 MJ/kg with a maximum burning velocity of \leq 10 cm/s A2L B2L No flame Propagation A1 **B**1 Lower Toxicity Higher Toxicity Flammability in Air @ 60°C & 101.3 kPa OEL $OEL \ge 400PPM$ < 400 PPM LFL = Lower Flammability Limit ETFL60 = Elevated Temperature Flame Limit @ 60°C HOC = Heat Of Combustion, OEL-Occupational Exposure Limit

ASHRAE Standard 34.1-2013-Toxicity/Flammability





- 1. ammonia is extremely hard (only above $650^{0}{\rm C})$ to ignite and breaks down above $450^{0}{\rm C}.$ The leaks are detectable above 5PPM by most. It is therefore extremely rare to encounter such high temperatures in normal air conditioning and refrigeration applications.
- 2. There is no reason for any concern that exposure to ammonia is a fire hazard.
- 3. Flammable limit by volume in air at atmospheric pressure for ammonia is as high as 16% to 25% concentration.
- 4. It is significant to know that no ammonia refigeration systems require use of flamproof controls by any International standard

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HIGHER	A3	B3
FLAMMABILITY	R-290 Propane	
	R-600a-Isonutane	
LOWER	A2	B2
FLAMMABILITY	R152a	
	A2L	B2L
	R-32	R-717 Ammonia
	R-1234yf	
	R1234ze(E))	
NO FLAME	A1	B1
PROPOGATION	R22, R134a, R410A,	R123
	R404A, R407C, R744-	
	CO ₂	

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Toxicity classifications

Class A signifies refrigerants where toxicity has not been identified at concentrations \geq 400 ppm v based on TLV-TWA data or consistent indices

Class B signifies refrigerants for where there is evidence of toxicity at concentrations < 400 ppm, based on TLV-TWA data or other consistent indices

TLV-Thresh hold limit value TWA-Time weighted average

Toxicity Levels of Ammonia refrigerant		
5 PPM	Onwards Detectable	
25 PPM	Detected by most – no health hazard exposure 10 – 15 years	
100 PPM	No dangerous effects, minor irritation.	
400 – 700 PPM	Irritation Eyes, Nose, Mucous . Lead to dryness	
1700 PPM	Cough, Cramp, Serious Irritation, Injuries	
2000 PPM	Can Lead to Death	
7000 PPM	Lethal within few minutes	
Recommended maximum allowable concentration for Ammonia in air is 2mg / m ³ for 30 minutes, 1mg / m ³ for 24 hrs & 0.5 mg / m ³ for one yearPPMx0,7=mg/m3		















Discharge Temperature with Operating conditions of+40°C/-20°C			
Refrigerant	Cp/Cv at boiling point or at Atmospheric pressure	Approximate isentropic Discharge Temperature ⁰ C	
R22	1.236	75	
R134a	1.154	55	
R404A	1.166	58	
R410A	1.244	70	
R717 (Ammonia)	1.348	145	

MATERIAL COMPATIBILITY

- 1. Ammonia is not compatible with copper and copper bearing alloys. It is fully compatible with iron, steel and aluminum and use of aluminum is on increase.
- 2. Since chlorofluorocarbons are compatible with all materials, any material can be chosen and thus provides greater flexibility.
- 3. Also Ammonia installtions use normally open drive motors since copper winding is not suitable for Ammonia

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FIELDS OF APPLICATIONS FOR AMMONIA REFRIGERANT

- The maximum allowable discharge gas temperature is 130-140°C with use of mineral oils for compressor lubrication.
- Many compressor manufacturers recommend use of synthetic oil for Ammonia systems designed for low temperature applications. The synthetic oil can withstand much higher temperatures say 140 to 150°C
- 3. If the isentropic temperature is exceeding this limit it is always advisable to go for multi-staging.
- 4. As a thumb rule if allowable temperature difference between saturated discharge and saturated suction temperature is more than 50K for Ammonia and 70K for R22 & other refrigerants, it is advisable to go for twostaging for getting better performance.

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OIL MISCIBILITY

 Ammonia and mineral oils are not miscible and oil travels with ammonia refrigerant and is thus present in all parts of the system. Oil therefore needs draining from various points-such as oil separator, Receiver, L.P. vessel, Oil pot, air coolers, flooded chiller etc.
 The problem can be substantially reduced if one uses efficient oil separators with demister s. s. pads , so that minimum oil goes into the system , and major portion can be drained automatically to compressor from oil separator.
 Miscible POE/PAG oils for DX systems are also now available
 Many engineers consider oil immiscibility as advantage since oil once drained from oil separator, the inner surfaces of heat exchangers

a remain clean and heat transfer improves compared to HFC/HCFC refrigerants. It is important to remember that oil is mainly required for compressor lubrication only and presence of oil elsewhere in the system is unwanted as oil does not give refrigeration or cooling effect.

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- Cold Storages for Potatoes, fruits ,vegetables and other commodities like chillies,seed storages,grains,termeric,dry fruits etc.
- 2. Ice Plants-Conventional block ice, flake ice, tube ice plants, slurry ice, plate ice plant
- 3. Fish freezing plants –Spiral freezers, plate freezers, IQF, Blast & Trolley freezers
- 4. Slaughter Houses & Meat processing plants
- Dairies using ice bank systems, ice reserve units ,chilled water systems, cold rooms and other requirements
- 6. Icecream making Plants
- 7. Chocolate making plants
- Process refrigeration plants using chilled water or low temperature brine chilling systems for Chemical/Dyestuff Industries
 Air conditioning of processing halls for cold chain facilities
- Air conditioning of processing halls for cold chain facilities like grading, sorting, Ante room areas.
 Breweries



11.Bottling plants for Coca-Cola/Pepsi & other soft drink bottlers 12. Concrete cooling applications for river dams, airport runways

and concrete expressways 13. Fertilizer plants Maximum use is of ammonia is in agricultural industry as a fertilizer with 99.5% minimum content of ammonia of commercial grade.

14. Recently many Super markets are also using ammonia/carbon dioxide(R717/R744) or ammonia/secondary fluids like propylene glycol systems

15. Liquefaction of gases like Chlorine,carbon dioixide & other gases

16. Pharmaceutical plants for process cooling

17. Mettalergical industry, ammonia is used as a source of inert gas, or for nitriding of metal surfaces.

18. In environmental protection, ammonia plays an important role in removing nitrogen oxides and sulpher dioxide from the smoke emitted by power plants.

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Non-Azeotropic Liquid Gas Blends-Advantage

- 1. Ammonia with Propane(290)
- 2. Ammonia with Octafluoropropane(R218)
- 3. Ammonia with Octafluorocyclobutane(R318)
- Ammonia with isobutane(R600a)
 60% Ammonia and 40% dimethyl ether(R723)

Experiments have shown that compared to pure Ammonia, some blends tested have lower discharge temperatures, lower compression ratios,5-10% better refrigeration capacity and better oil solubility(PAG or PAO oils),and reduces toxicity

Ref: Monika Witt-Condenser magazine November 2008

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19.Air conditioning of large complexes like Air ports, telegraph, and other commercial office premises – more details given subsequently, using chilled water systems.
20. Skating ice rings for amusement parks
21. Space shuttles
22. Heat Pumps. Industrial heat pumps
23. Marine Refrigeration
and many other not listed applications

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THANK YOU Questions?

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